




Radio-Frequency Coulomb-Blockade Thermometry

Florian Blanchet,^{*} Yu-Cheng Chang^{ib}, Bayan Karimi^{ib}, Joonas T. Peltonen^{ib}, and Jukka P. Pekola^{ib}[†]
*Pico group, QTF Centre of Excellence, Department of Applied Physics, Aalto University, P.O. Box 15100, Aalto
FI-00076, Finland*

 (Received 24 September 2021; revised 19 November 2021; accepted 10 December 2021; published 26 January 2022)

We present a scheme and demonstrate measurements of a Coulomb-blockade thermometer (CBT) in a microwave-transmission setup. The sensor is embedded in an LCR resonator, where R is determined by the conductance of the junction array of the CBT. A transmission measurement yields a signal that is directly proportional to the conductance of the CBT, thus enabling the calibration-free operation of the thermometer. This is verified by measuring an identical sensor simultaneously in the usual dc setup. The important advantage of the rf measurement is its speed: the whole bias dependence of the CBT conductance can now be measured in a time of about 100 ms, which is 1000 times faster than in a standard dc measurement. The achieved noise-equivalent temperature of this rf primary measurement is about $1 \text{ mK}/\sqrt{\text{Hz}}$ at the bath temperature $T = 200 \text{ mK}$.

DOI: [10.1103/PhysRevApplied.17.L011003](https://doi.org/10.1103/PhysRevApplied.17.L011003)

Deep Coulomb Blockade



Coulomb blockade thermometer

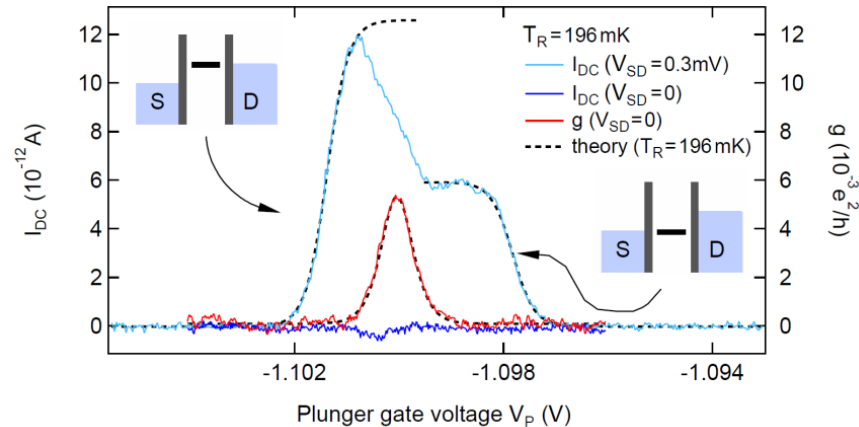
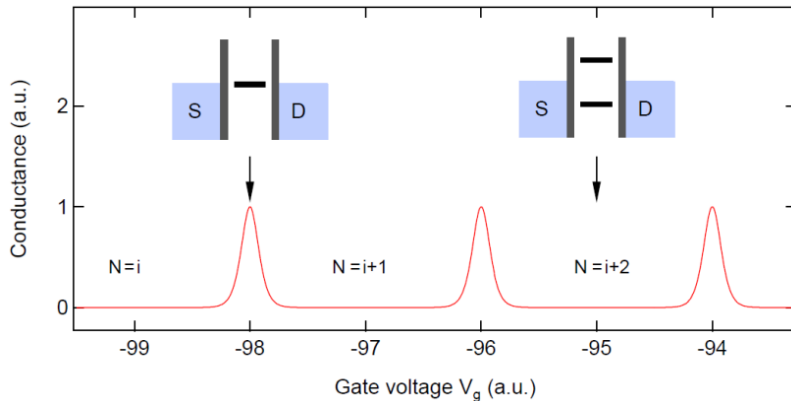
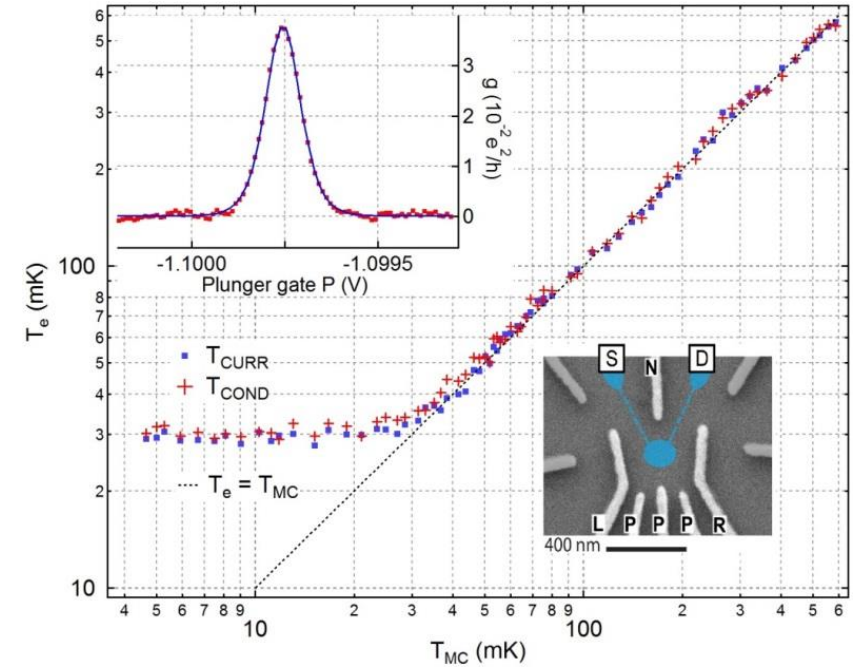
Coulomb blockade

- Isolated charge, Capacitance to environment \Rightarrow charging E_C
- Energy $eV \sim$ Temperature $k_B T$
- Tunnel rate: $\delta E \cdot \delta t > h$ (charging time RC , energy $E_C = e^2/C \Rightarrow R \sim 25.8 k\Omega$)

Deep Coulomb blockade $k_B T \ll E_C$

Thermometry requirement

- Tunnel rate: $\Gamma \ll \frac{k_B T}{h}$ (small currents at low T !!!)
- AC measurement: $eV \ll k_B T$



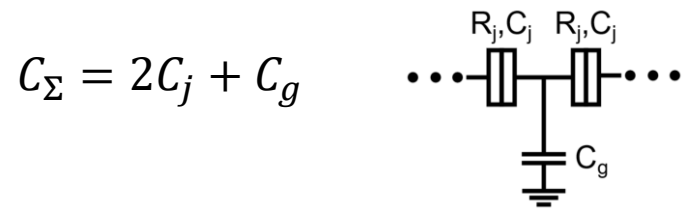


Weak Coulomb Blockade



CBT: Coulomb blockade thermometer

- 2D Array of “small” metal islands with tunnel-junctions in-between
- Finite Capacitance $C_\Sigma \Rightarrow E_C = \frac{e^2}{2 \cdot C_\Sigma}$ Energy eV \sim Temperature $k_B T$
- For $T \gtrsim E_C$ zero bias suppression (charging effects)



Universal regime

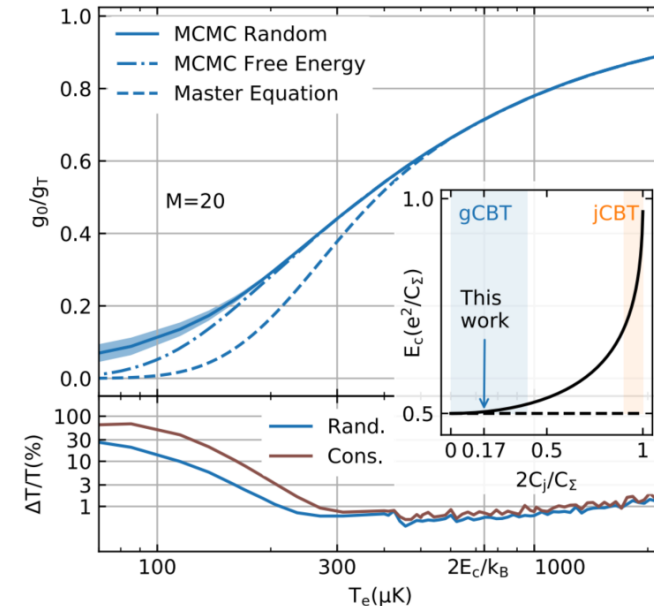
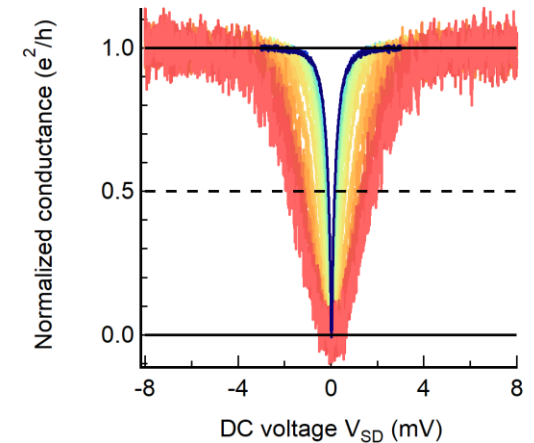
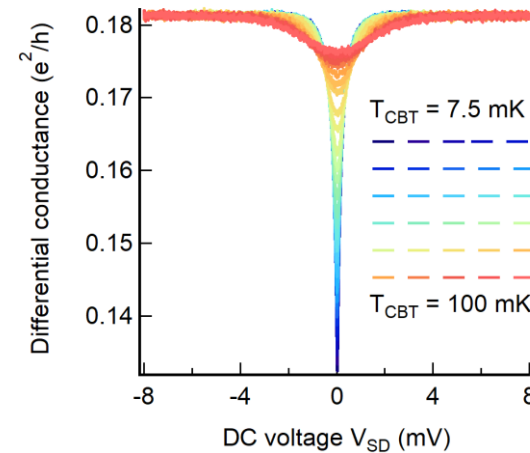
- No gate for CBT islands \Rightarrow “random” offset charge on each island
- For $k_B T > 0.8 E_C$ universal conductance suppression

Primary thermometer:

- Width $eV_{1/2} = 5.4392 N k_B T$ (in absence of bias heating)

Secondary mode operation:

- Depth $\delta g \approx \frac{1}{6} u - \frac{1}{60} u^2 + \frac{1}{630} u^3$; $u = \frac{2E_C}{k_B T}$ (high-T calibration \rightarrow charging energy EC)



RF CBT setup

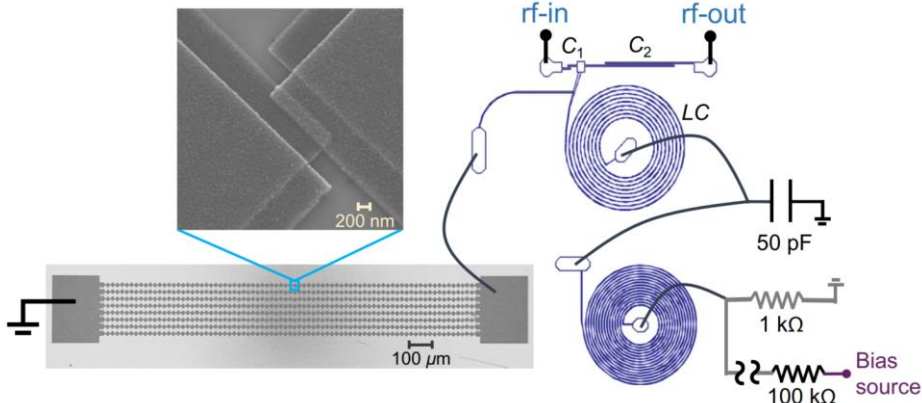


CBT Devices

| | | | |
|-----------------------------|---------|----|----------------------|
| CBT100_dc: 100 k Ω , | classic | DC | 100 junction, 10 row |
| CBT80_dc: 80 k Ω , | AlMn | DC | 80 junction, 8 row |
| CBT80_rf: 80 k Ω , | AlMn | RF | 80 junction, 8 row |

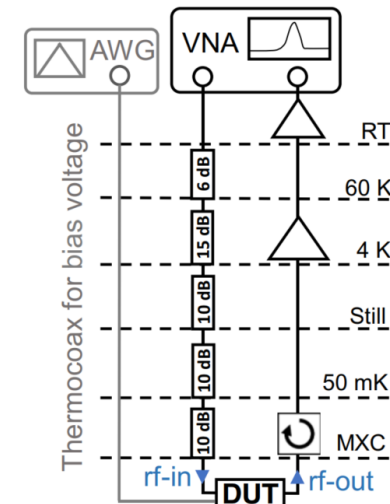
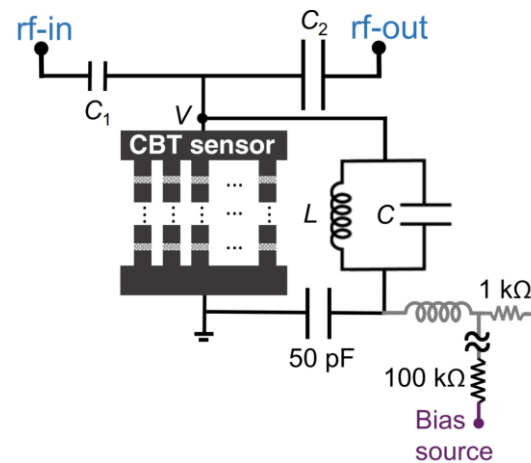
LCR tank circuit

- Tank: $f_0 = 547$ MHz, $Q = 45$, $t_R = (Q/2\pi f_0) = 13$ ns
- Nb inductor: $L = 110$ nH (200nm sputtered onto high-R Si wafer)
- Capacitance: $C = 540$ fF ($C_1 = 67$ fF, $C_2 = 170$ fF)
- Attenuation: 51dB (all stages \rightarrow thermalization)
- Amplification: HEMT @ 4.2K
- Circulator: 480-720MHz BW, 20dB isolation
- Drain: CBT hard ground at LT



Sample fabrication

- 2 angle shadow mask patterned by e-beam
- Alloy target with 0.3% nominal Mn concentration
- Sequence:
 - 20nm film of alloy, -45° tilt
 - in-situ oxidation (pure O₂, 10min)
 - 30nm film of alloy, $+45^\circ$ tilt
- Overlapp (junction): $1,2\mu\text{m} \cdot 180\text{nm}$
- Island: $15\mu\text{m} \cdot 15\mu\text{m}$
- Small island + weak ep-coupl. in AlMn
 \Rightarrow operation limited to $T > 200\text{mK}$ (overheating)





RF vs DC transport



RF measurement

Transmitted signal:

$$S_{21} = S_0 - 20 \lg(1 + R_0 G)$$

$$R_0 \approx [R_L (2\pi f_0 C_2)^2]^{-1} \approx 59 \text{ k}\Omega$$

$$R_L \approx 50 \Omega$$

Linearize for $dg/g \ll 1$:

$$S_{21} = \tilde{S}_0 - \frac{20}{\ln(10)} \frac{R_0 G_T}{1 + R_0 G_T} \frac{G(V)}{G_T}$$

Precision: $1 \text{ mK}/\sqrt{\text{Hz}}$

\Rightarrow 2% precision @ 200 mK in 100ms

DC + Fit in inset:

Conductance dip with CBT fit $\rightarrow T_e, E_C$

$$G(v)/G_T = 1 - u g(v)$$

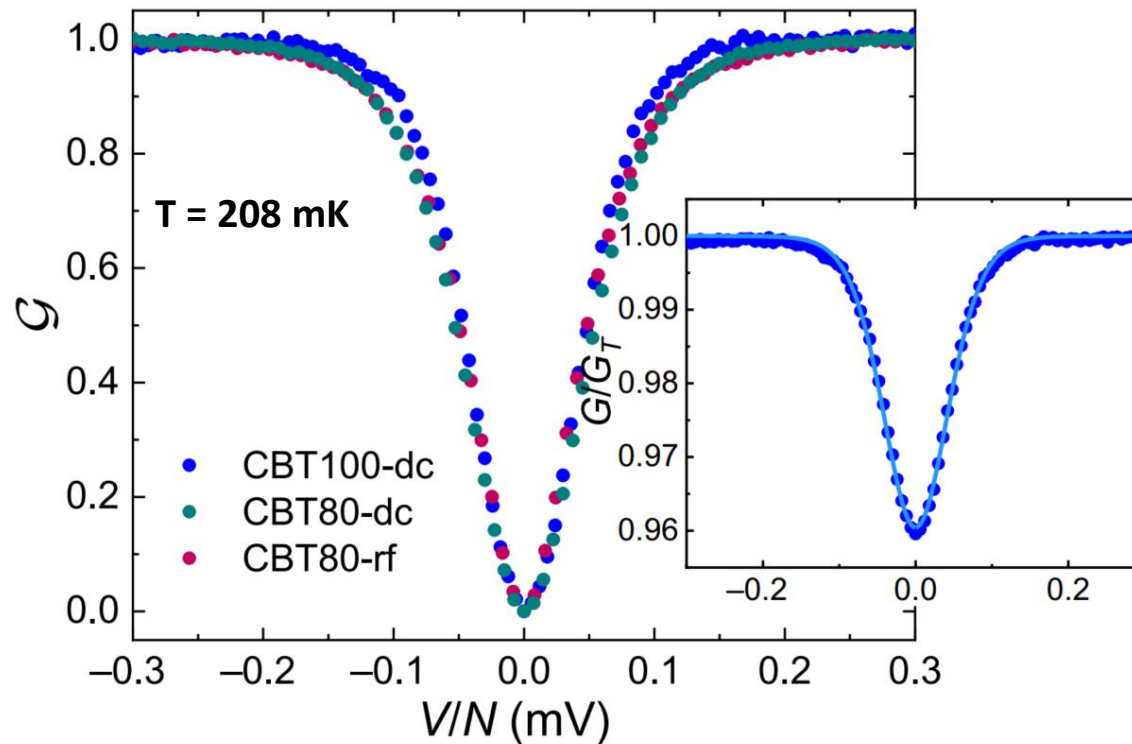
$$- \frac{u^2}{4} [g'(v)h'(v) + g''(v)h(v)]$$

$$g(v) = e^v [e^v (v - 2) + v + 2] / (e^v - 1)^3$$

$$u = E_C / (k_B T)$$

$$v = eV / (Nk_B T)$$

$$h(v) = v \coth(v/2)$$



$$\text{Normalized conductance: } G' = \frac{G(V) - G(0)}{G_T - G(0)}$$



Motivation

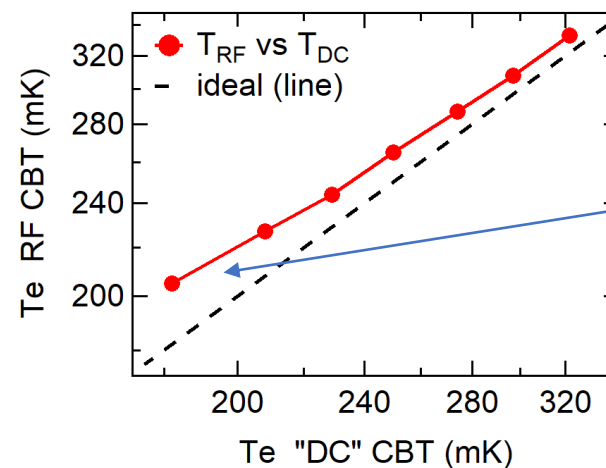
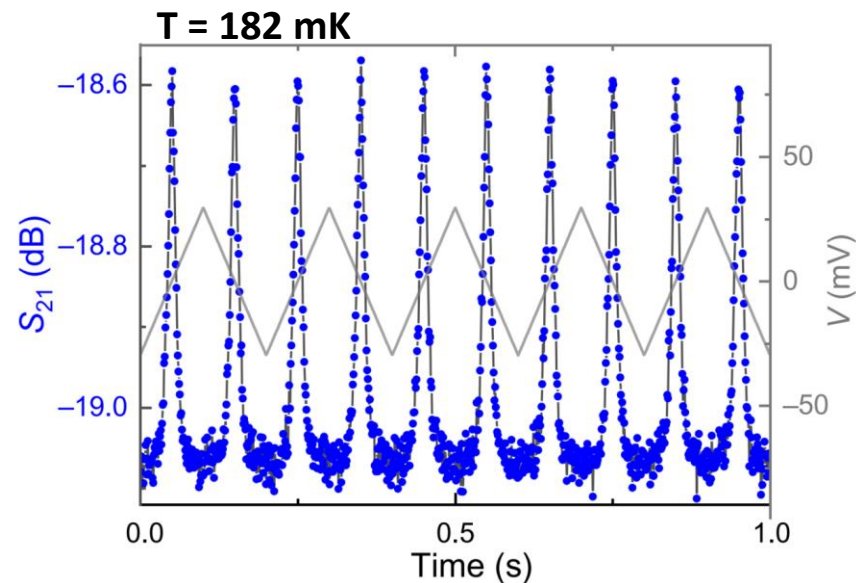
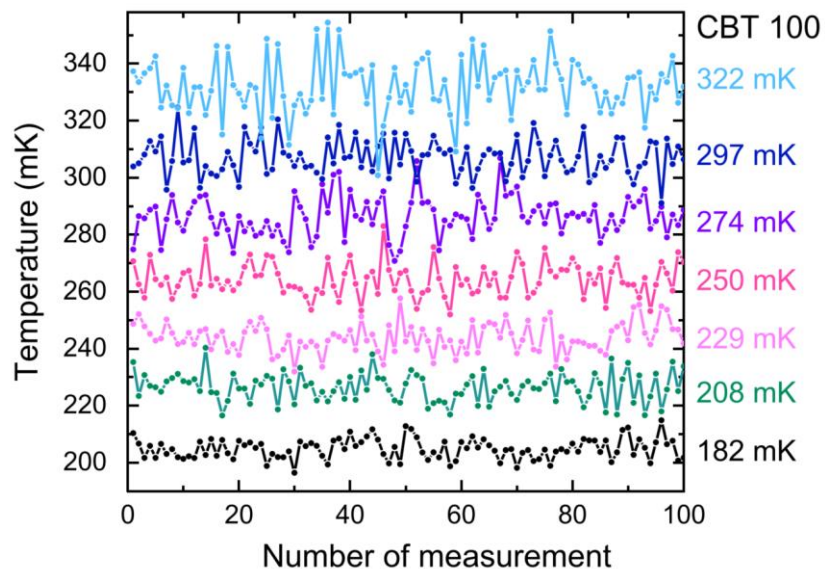


Fast DC bias-scans

- Triangular $\pm 30\text{mV}$ voltage ramp across device (AWG, 100ms half period)
- Sign inverted in S_{21} : dip \rightarrow peak

RF vs "DC" temperature

- Qualitative agreement
- RF reads higher in general (RF heating effects ?)
- Plot T_{RF} vs T_{DC} would be nice !



Separation:
RF heating ?



Summary



- CBT measured @ 200 - 350 mK with tank circuit (547MHz)
- 100 ms acquisition time for DC sweep (1000 times faster)
- “Good” agreement between DC and RF measurement
- Probably overheating with RF (needs more work to be useful at low T)
- AlMn tunnel junction CBT developed: Works also at B=0 !!! (interesting for AND)